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(21) International Application Number: PCT/FI93/00233 (22) International Filing Date: 31 May 1993 (31.05.93) (30) Priority data: 922520 29 May 1992 (29.05.92) FI (71) Applicant (for all designated States except US): NESTE OY [FI/FI]; Keilaniemi, FIN-02150 Espoo (FI). (72) Inventors; and (75) Inventors/Applicants (for US only) : HEINO, Markku [FI/FI]; Maasälväntie 14 B 44, FIN-00710 Helsinki (FI). SEPPÄLÄ, Jukka [FI/FI]; Rantakieventie 18 as. 6, FIN-00960 Helsinki (FI). WESTMAN, Marjut [FI/FI]; Kuunsirppi 2 A 8, FIN-02210 Espoo (FI).		(74) Agent: SEPPO LAINE KY; Lönnrotinkatu 19 A, FIN-00120 Helsinki (FI). (81) Designated States: JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report. In English translation (filed in Finnish).</i>
(54) Title: LIQUID CRYSTAL POLYMER BLENDS, PROCESS FOR THE PREPARATION THEREOF AND PRODUCTS MANUFACTURED FROM THE BLENDS (57) Abstract The invention relates to a polymer blend, a process for the preparation thereof and products manufactured from the polymer blend. The polymer blend contains 95 to 50 parts by weight of a polyolefin- or polyester-based polymer matrix, 5 to 50 parts by weight of an aromatic main-chain liquid crystalline polymer, and plastic additives, if any. Further, the blend contains, based on the total weight of the previous components, 0.1 to 30 per cent by weight of a substance (a compatibilizer) which improves the compatibility of the polymer matrix and the liquid crystalline component. According to the invention, the compatibilizer comprises a polymer containing reactive, functional groups. Preferably the compatibilizer comprises a SEBS polymer functionalized with maleic anhydride or an olefin polymer functionalized with glycidyl methacrylate. Having excellent tensile, flexural and impact strength, the polymer blends according to the invention, can be used for the manufacture of tubes, pipes, sheets and fibres. They are suited, e.g., for manufacture of constructional parts of electrical and optical cables.		

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LIQUID CRYSTAL POLYMER BLENDS, PROCESS FOR THE PREPARATION THEREOF
AND PRODUCTS MANUFACTURED FROM THE BLENDS.

5 The present invention concerns a liquid crystalline blend
according to the preamble of claim 1.

10 This kind of a blend comprises a polymer matrix and a liquid
crystalline polymer. The blend further contains a substance
which enhances the compatibility of the polymer matrix and
the liquid crystalline polymer.

15 The invention also relates to a process according to the
preamble of claim 13 for preparing liquid crystalline polymer
blends and to products according to claims 18 and 19, which
essentially consist of said polymer blends.

20 Liquid crystalline polymers are polymers which in melt state
lie between the boundaries of solid substances and liquids.
The liquid crystalline structure is called a mesomorphic
phase or an anisotropic phase because macroscopically in the
melt state the liquid crystalline polymers are fluids. Micro-
scopically they have a regular structure similar to that of
crystals. The liquid crystalline polymers are called "thermo-
25 tropic" if their anisotropy depends on the temperature only.
The strength and stiffness of many thermoplastics can be
substantially improved by blending them with thermotropic,
main-chain liquid crystalline polymers. This is because the
liquid crystalline polymers form fibres which orientate in
30 the flow direction of the thermoplastic matrix melt. As a
result there is an improvement of the mechanical properties,
such as tensile strength and modulus of elasticity, of the
thermoplastic in this direction. Often, the addition of the
liquid crystalline polymer also improves the heat resistance
35 and dimensional stability of the thermoplastics and makes it
easier to process them.

The above-mentioned polymer blends are, however, hampered by the problem that their transversal properties, such as impact strength, are inferior to those of the corresponding unblended plastics. This phenomenon is due to the anisotropic structure and to the poor adhesion between the liquid crystalline polymer phase and the thermoplastic phase.

It is known in the art that the compatibility of liquid crystalline polymers and thermoplastics and that the impact strength of blends thereof can, to some extent, be improved by adding to the blends a third component, i.e. a substance known as a compatibilizer. The task of the compatibilizer is, for instance, to diminish surface tension between the phases, to improve adhesion, and to improve dispersion.

EP Published Patent Application No. 0 369 734 describes a polymer blend which consists of a poly(alkylene terephthalate) matrix, a polyacrylate-based liquid crystalline polymer and a substance which improves the impact strengths of the processed articles at low temperatures. According to the reference, the last-mentioned substance can be comprised of polyethylene, polypropylene, an ethylene-acrylic acid copolymer or a ethylene-propylenediene rubber.

A compatibilized blend of a liquid crystalline polymer and polycarbonate is disclosed in the EP Published Patent Application No. 0 380 112. The compatibilizer used in said reference consists of a polyolefin and/or olefinic copolymers. Among the olefinic copolymers, substances containing styrene monomers may be mentioned.

Common to both of the embodiments described in the references above is that the impact strength improvements of the polymer blends have been rather small.

The present invention aims at removing the problems relating to the prior art while providing liquid crystalline polymer

blends of an entirely novel kind.

Our invention is based on the concept that the substance used for promoting the compatibility of the polymers comprises a polymer containing reactive functional groups. Surprisingly, it has been found that by adding polymers containing reactive groups to blends comprising thermoplastics and liquid crystalline polymers it is possible to provide polymer blends, with tensile and flexural strength properties which are better than the corresponding properties of the polymer matrix, while the impact strength remains at least reasonably good as far as practical applications are concerned. Thus, the impact strengths of the polymer blends according to the invention are at least 20 % better than the impact strengths of corresponding uncompatibilized blends.

In particular, the blend according to the invention is mainly characterized by what is stated in the characterizing part of claim 1.

The process according to the invention is characterized by what is stated in the characterizing part of claim 13.

For the purpose of this application the term "reactive compatibilizer containing functional groups" denotes a polymer which at least in principle is capable of reacting with at least one of the components of the blend. In practice it is difficult to determine the exact nature of the interaction between the compatibilizer and the other components of the blend, to ascertain whether a chemical reaction has taken place or not. Therefore, within the scope of the present application, all polymers which contain functional groups capable of reacting with the functional groups of the matrix polymer and/or the liquid crystalline polymer, are considered to be reactive compatibilizers. In blends containing polyolefins, the reactive, functional groups of a polymer working as a compatibilizer react (or

interact in some other way) with the functional groups of the liquid crystalline polymer. Generally, the last-mentioned groups are comprised of the free terminal groups of the polymer chain. The polymer chain of the compatibilizer (e.g.
5 its polyolefin residue) interacts with the polyolefinic matrix without there necessarily being any chemical reaction. In blends containing polyesters, such as poly(ethylene terephthalate) (PET) and poly(butylene terephthalate) (PBT), and a liquid crystalline polymer, the compatibilizer may
10 react both with the matrix and with the liquid crystalline polymer because PET, for instance, is not an entire inert polymer.

The functional groups of the compatibilizer comprise, for
15 example, carboxy, anhydride, epoxy, oxazolino, hydroxy, isocyanate, acylacetam and carbodiimide groups.

The polymer residue of the compatibilizer can comprise co- and terpolymers, grafted polyolefins, grafted polystyrene and
20 thermoplastic elastomers. The polar groups of polyolefinic copolymers are generally acrylic esters or functional acrylic acid groups. The polar groups of the terpolymers can be maleic anhydride groups, hydroxyl groups and epoxy groups, of which the last-mentioned are particularly preferred. The
25 styrene block copolymers can consist of polystyrene segments and flexible elastomer segments. Typical styrene block copolymers are SBS (styrene/butadiene/styrene-copolymer), SIS (styrene/isoprene/styrene-copolymer) and SEBS (styrene/ethylene butylene/styrene-copolymer).

30 The compatibilizer used is selected depending on the other components of the liquid crystalline polymer blend. According to the present invention, particularly preferred compatibilizers are functional polyolefines or olefinic
35 copolymers (including styrene), the functional groups preferably being epoxy, carboxy, amine or hydroxyl groups, in particular epoxy groups and glycidyl methacrylate groups. The

portion of functional groups in the polymer is about 0.1 to 30 %, preferably 1 to 10 %.

"Liquid crystalline polymer blend" means a blend in which at least one thermoplastic has been blended with at least one liquid crystalline polymer. The blend further contains at least one of said compatibilizers and additives, if any. The blending of a liquid crystalline polymer with a thermoplastic gives rise to a blend whose viscosity generally is smaller than the viscosity of the thermoplastics. The blend of a liquid crystalline polymer and thermoplastics can also be called an "in situ" blend because the liquid crystalline polymer fibres are formed first during processing of the blend.

The plastic matrix stock of the polymer blend can comprise any suitable polymer material which has the desired properties as regards strength and processability. As examples of the matrix polymers, the following polymers may be mentioned: polyolefins such as polyethylene, polypropylene, polybutylene, polyisobutylene, poly(4-methyl-1-pentylene), including copolymers of ethylene and propylene (EPM, EPDM) and chlorinated and chlorosulphonated polyethylenes. The matrix polymer may also be comprised of the corresponding polyalkanes, which contain styrene, acryl, vinyl and fluoroethylene groups, and different polyesters, such as poly(ethylene terephthalate), poly(butylene terephthalate) and polycarbonate. Particularly preferred matrix polymers are the polyolefins and polyesters. In the example described below polypropylene and poly(ethylene terephthalate) have been used as matrix polymers. However, equally preferred are polyethylene and poly(butylene terephthalate). Together with a polypropylene matrix it is, according to the invention, particularly advantageous to use a ethylene-terpolymer having glycidyl methacrylate groups, and together with a poly(terephthalate ester) the same terpolymer or, alternatively, maleic anhydride grafted SEBS.

The liquid crystalline polymer may comprise an aromatic main chain thermotropic polymer, preferably a thermotropic polyester, poly(ester amide), poly(ester ether), poly(ester carbonate) or poly(ester imide). It can also comprise a
5 copolymer of a polyester, such as a copolymer of poly(ethylene terephthalate) and hydroxy benzoic acid or a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid. Generally, the liquid crystalline polymer can be defined as a polymer which is formed when the components of the following
10 general formulas (or at least two of them) are reacted with each other: a dicarboxylic acid of formula $\text{HOOC-R}_1\text{-COOH}$, a diol of formula $\text{HO-R}_2\text{-OH}$, and an oxycarboxylic acid of formula $\text{HO-R}_3\text{-COOH}$, wherein R_1 , R_2 and R_3 represent a bivalent aromatic hydrocarbon group, a group of formula $\text{R}_4\text{-X-R}_5$, wherein R_4 and
15 R_5 represent a bivalent hydrocarbon group and X is an oxygen or a sulphur atom, a sulphonyl, carbonyl, alkylene, or ester group or X is a single bond, a xylylene group or a bivalent aliphatic hydrocarbon group. The liquid crystalline polymer can also comprise a homopolymer of an oxycarboxylic acid of
20 formula $\text{HO-R}_3\text{-COOH}$.

As far as liquid crystalline polymers and their properties are concerned, reference is made to the article by Chung et al. in Handbook of Polymer Science and Technology, Vol. 2
25 (1989) 625 - 675.

Of the polymer blend additives, fillers, pigments and various substances which promote the processing of the blend can be mentioned.

30 In the liquid crystalline polymer blend the proportion of the liquid crystalline polymer may, in principle, vary within large ranges, depending on the effect which is sought to be achieved by the liquid crystalline polymer addition. Said
35 proportion calculated on basis of the total amount of the matrix polymer, and the liquid crystalline polymer may vary in the range from 1 to 99 %. By adding about 1 to 15 percent

by weight of a liquid crystalline polymer to the matrix polymer a decrease of the viscosity is obtained which enhances the processing. By adding about 15 to 85 percent by weight self-enforcing plastics are provided, whereas an amount of 85 to 99 percent by weight will give rise to modified liquid crystalline polymers. According to the invention there are, however, preferably prepared liquid crystalline polymer blends, in which the amount of the liquid crystalline polymer lies in the range from about 5 to about 50 percent by weight, in particular about 10 to about 30 percent by weight of the total amount of the matrix polymer and the liquid crystalline polymer. The corresponding amount of the matrix polymer is preferably about 95 to about 50 percent by weight, in particular about 90 to about 70 percent by weight. The amount of the compatibilizer can vary in the range from about 0.1 to 30 %, preferably it is about 1 to 15 percent by weight of the total weight of the matrix polymer and the liquid crystalline polymer. These relative amounts of the components will provide a reinforced plastic, in which the reinforcement is comprised of the liquid crystalline polymer.

Plastic additives known per se can be added to the polymer blend according to the invention. These additives comprise, for instance, stabilizers, colouring agents, lubricants, antistatic agents, fillers and fire retardants. If desired, these substances can be premixed with, e.g., the matrix polymer before forming the polymer blend. The amounts of polymer additives are typically about 0.01 to 5 %, preferably about 0.1 to 2 % of the weight of the polymer blend.

Of the liquid crystalline polymer blends according to the invention, the following are particularly preferred:

A. Polypropylene (PP) matrix, a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid as a liquid crystalline polymer (LCP) and, as compatibilizer (comp. D), a

ethylene-terpolymer, containing glycidyl methacrylate and epoxy groups. The following preferred blend compositions may be mentioned:

- 5 A1 about 70 parts by weight of PP, about 30 parts by weight of LCP and 5 to 10 percent by weight of comp. D (calculated on basis of the weight of PP and LCP) and
- A2 about 90 parts by weight of PP, about 10 parts by weight of LCP and 2 to 5 percent by weight of comp. D (calculated on basis of the total weight of PP and
- 10 LCP).

B. Poly(ethylene terephthalate) (PET) matrix, otherwise the same components as under point A. The following example of the preferred blend compositions may be mentioned:

- 15 B1 about 90 parts by weight of PET, about 10 parts by weight of LCP and 2 to 5 percent by weight of comp. D (calculated on basis of the total weight of PET and LCP).

20 C. Poly(ethylene terephthalate) (PET) matrix, a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid as a liquid crystalline polymer (LCP) and, as a compatibilizer (comp. A), maleic anhydride grafted SEBS. The following example of the preferred blend composition may be mentioned:

- 25 C1 about 90 parts by weight of PET, about 10 parts by weight of LCP and 5 to 10 percent by weight of comp. A (calculated on basis of the total weight of PET and LCP).

30 Particularly preferred matrix polymer/liquid crystalline polymer blends are represented by those having better tensile and flexural strengths than the matrix polymer and having at least 20 % better impact strength than the uncompatibilized polymer blends. Thus, the Charpy impact strength of unnotched

35 test samples prepared from blends according to the invention is typically over 30 kJ/m².

The thermoplastic/liquid crystalline polymer blends according to the invention can be prepared by methods known per se.

The mixing methods are either batch or continuous processes. As examples of typical batch mixers, the Banbury mixer and the heated roll mill may be mentioned. Continuous mixers are exemplified by, for instance, the Farrel mixer, and single- and double-screw extruders. Preferably single- or twin-screw extruders are used for blending the liquid crystalline polymer with the thermoplastic. The liquid crystalline polymers are blended with the thermoplastics either by first premixing the liquid crystalline polymers with the thermoplastics in a twin-screw extruder and then processing them in an injection moulding machine or, alternatively, by processing them by injection moulding or extrusion without premixing.

The blends according to the invention can be processed according to methods known per se in polymer technology to manufacture the final products. Thus, the blends can be used for preparing moulded articles, extruded products and thermoformed products. The moulded articles can be manufactured by, for instance, injection moulding or blow moulding. Fibres, films, pipes, profiles, cables and coatings may be mentioned as examples of extruded products.

Because, as mentioned above, the liquid crystalline polymer blends are "in situ" blends it is particularly preferred to process the blends by extrusion, LCP fibres being formed during extrusion, which improves the strength properties of the products in longitudinal direction. According to a preferred embodiment of the invention, extrusion is used to manufacture liquid crystalline polymer blends consisting of a polypropylene matrix.

By using rotating dies or similar methods it is possible to achieve not only longitudinal reinforcement of products

prepared by extrusion but also transversal reinforcement. The biaxial orientation thus obtained is particularly preferred when liquid crystalline polymer blends are used for manufacturing certain products.

5

Considerable advantages are achieved by the polymer blends according to the invention and by their use for various applications.

10

Thus, it is possible to obtain a substantial improvement of the impact strength of liquid crystalline polymer blends by compatibilizer addition. Since, however, an increase of the compatibilizer portion at the same time to some extent impairs the longitudinal strength of the blends, as the

15

examples below show, it is preferred according to the invention to add only so much amounts of the compatibilizer that the tensile strength and the flexural strength of the blend still are better than the corresponding properties of the polymer matrix.

20

As an example of the improvement of the impact strength obtainable by the present invention, it may be mentioned that the Charpy impact strength of an injection moulded liquid crystalline/polypropylene blend (30/70) was three-folded when

25

a small amount of ethylene based terpolymer was added. The melt flow viscosity of the blend was also slightly increased after the addition of the compatibilizer, which appears to indicate that the compatibilizer addition not only improves the impact strength but it also increases phase interaction.

30

Following the compatibilizer addition, the size of the liquid crystalline polymer phases decreased, which indicates that the compatibilizers according to the invention increases dispersion.

35

Consisting only of thermoplastics, the reinforced plastics and the products prepared from them can be recirculated as such because they do not contain reinforcing fibres

consisting of other materials, such as glass. The wear of the processing equipment is, for the same reason, diminished. Processability is improved and because there is not much thermal expansion, instrument parts requiring dimensional stability can be manufactured from the blends. Due to the small temperature coefficient, the blends are well suited for use as constructional materials for electrical and optical cables.

With reference to what is stated above, the present invention concerns, in particular, constructional parts of electrical and optical cables manufactured from the above-mentioned liquid crystalline polymer blends.

The blends can also be used for manufacturing injection moulded parts used in the electronics industry. Pipes and tubes made from the blends typically have good barrier properties, i.e. low permeability.

In the following the invention is described more closely with the help of a detailed description and non-limiting working examples. In the working examples reference is made to the attached drawings, of which

Figure 1 shows a SEM micrograph of the cross section of a PP/30 wt.-% LCP blend prepared in a Brabender-melt mixer, a) without any compatibilizer and b) with 7 wt.-% of compatibilizer D, D),

Figure 2 shows the modulus of elasticity as a function of the draw ratio for extruded blends of PP/LCP/compatibilizer D, Figure 3 shows the melt viscosities for PP, PP/LCP (70/30) and PP/LCP(70/30)/10 wt.-% of compatibilizer D blends as a function of the shear rate at 290 °C;

Figure 4 shows SEM micrographs of the cross section of a) a PP/EPDM (75/25) compound and b) PP/18 % EPDM/ 30 % LCP blend, Figure 5 indicates the influence of compatibilizers on the Charpy impact strength of a PET/LCP 10 blend,

Figure 6 indicates the influence of compatibilizers on the flexural strength of a PET/LCP 10 blend,

Figure 7 indicates the influence of compatibilizers on the maximum tensile strength of a PET/LCP 10 blend,

5 Figure 8 shows SEM micrographs of binary blends of LCP and compatibilizers: a) PP/compatibilizer D, b) LCP and compatibilizer D, and c) LCP and compatibilizer A,

Figure 9 illustrates the influence of the compatibilizer on the melt viscosity of a binary LCP blend, and

10 Figure 10 shows SEM micrographs of cross sections of extruded strands made from compatibilized polymer blends: a) PET/30 % LCP/5 % comp. D, b) PET/30 % LCP/7.5 % comp. A and c) PP/30 % LCP/5 % comp. D.

15 MANUFACTURING PROCESS

1. General

Thermotropic main-chain liquid crystalline polymer (LCP) was
20 blended with thermoplastics, the amount of the LCP being 10 to 30 percent by weight of the weight of the blend (without the compatibilizer). In order to improve the compatibility of the components of the blend, small amounts of different compatibilizers were added to the LCP/thermoplastic blends.
25 The blend processed in a twin-screw extruder were injection moulded to test samples whose mechanical and thermal properties as well as morphology and rheology were tested.

Example 4 discloses a new way of preparing compatibilized
30 liquid crystalline polymer blends according to which embodiment the compatibilizer is first preblended with the liquid crystalline polymer, the thermoplastic being added in the second stage of the process. By the process an improved interaction between the compatibilizer and the LCP is
35 achieved.

2. Materials

The liquid crystalline polymer used was a PHB/HNA based aromatic copolymer marketed under the trade name Vectra A 950. This product is supplied by Hoechst Celanese and its density is 1.40 g/cm³, melting point 280 °C, tensile strength 165 MPa, elastic modulus 9700 MPa, and elongation at break 3.0 %. It consists of a copolymer of hydroxynaphthoic acid and p-hydroxybenzoic acid

Homopolymer VB 19 50K supplied by Neste Oy was used as polypropylene, and the crystallizing product Arnite D04 300 supplied by AKZO as poly(ethylene terephthalate).

The compatibilizer used comprised a reactive ethylene-based terpolymer (compatibilizer D) marketed under the name Lotader AX 8660. The polymer is supplied by Atochem. The product contains about 30 percent by weight of ethyl acrylate, 62 percent by weight of ethene, and 8 percent by weight of glycidyl methacrylate having reactive epoxy groups. The other reactive compatibilizer used comprised maleic anhydride grafted SEBS with an acid content of 1.8 percent by weight (compatibilizer A). The product is supplied by Shell under the name Kraton FG 1901 X. The afore-mentioned compatibilizers were added in amounts of 2 to 10 percent by weight of the amount of the thermoplastic and LCP blend.

In the reference test, an improvement of the impact strength of PP/LCP blends were attempted by adding non-functional EPDM rubber (Keltan 778 DSM) to the blend and by blending LCP with a PP/EPDM (75/25) compound (DE 2561 Neste). Also non-functional SEBS polymer was used.

3. Blending

Before the melt blending stage the materials were first manually mixed with the matrix thermoplastics as dry pellets.

The mixed polymer pellets were then dried. The drying conditions for the blends were chosen according to the matrix polymers and were normally at least 2 hours at 70 °C.

5 The melt blending of the materials was performed by a Berstorff ZE 25x33D co-rotating twin-screw extruder at temperatures ranging from 285 to 290 °C (the temperature of the molten polymer was about 290 to 295 °C) and with a screw speed of 150 rpm. The extrudate was immediately quenched in a
10 water bath and pelletized again.

4. Injection moulding

The blends as well as the pure polymers were dried as
15 described above and injection moulded into the form of test specimens. Pure thermoplastic polymers were processed at typical conditions (the polypropylenes at about 210 to 230 °C). The blends were injection moulded at about 280 to 290 °C.

20

5. Extrusion

Some blends were extruded to strands with a Brabender Plasti-Corder PLE 651 laboratory single screw extruder
25 connected after the water basin to a belt capstan. The extrudate was drawn at different speeds to give a picture of the influence of the draw ratio on the properties of the strand (LCP orientation). The draw ratio for each strand was determined as the ratio between the die and the strand
30 cross-sections. The cylinder temperatures of the extruder were 280 to 285°C. The diameter (D) of the round hole capillary die was 5 mm and the capillary length (L) 30 mm, thus the L/D ratio was 6. The speed of the belt capstan ranged from 10 to 40 m/min.

35

The twin screw extruder used comprised a Brabender DSK 42/7 counterrotating twin-screw extruder. The temperature was

maintained at about 230 to 290 °C with a screw speed of about 75 rpm.

CHARACTERIZATION OF THE BLENDS

5

Before testing, all samples were conditioned applying ISO 291 at test room conditions (about 23 °C and 50 % relative humidity) for at least 88 hours.

10

1. Mechanical properties

The mechanical properties of the blends were assessed by testing the blends for tensile strength, flexural strength and impact strength.

15

Tensile properties were measured according to ISO 527. Flexural properties were studied with the same equipment according to ISO 178 as a three-point-bending test. Charpy impact strength was determined of unnotched test specimens according to ISO 179 by using a Zwick 5102 pendulum type testing machine. A pendulum of 40 kpcm was used.

20

2. Other properties

25

The morphology of the blend samples was investigated with a scanning electron microscope (SEM).

30

The rheology of the polymers was investigated by measuring their melt viscosities in shear flow. The measuring temperature was 290 °C and the L/D ratio of the die was 20 mm/0.5 mm. Bagley correction was not done but the results include Rabinowitch correction.

Example 1**Compatibilized PP/LCP blends**

5 Polymer blends were prepared from PP homopolymer and LCP, and
2 to 10 percent by weight of a reactive ethylene based
terpolymer (comp. D) was added to the blends. Processing,
injection moulding and testing of the blends were carried out
as described above.

10 The results obtained are indicated in Table 1. The
abbreviations used in the table, for instance PP/20/D 3,
relate to the compositions of the liquid crystalline polymer
blend compositions, PP/20/D 3 indicating that the relation
between PP and LCP in the blend amounts to 80:20 and there is
15 3 percent of substance D calculated on basis of the total
weight of the PP and the LCP.

Table 1. Mechanical properties of injection moulded compatibilized PP/LCP blends

	Material	TENSILE PROPERTIES		FLEXURAL PROPERTIES		IMPACT STRENGTH	
		E (MPa)	σ (MPa) / ϵ (%)	E (MPa)	σ (MPa)	Charpy (kJ/m ²)	
10	PP	1047	/ 24.0 / >100	964	/ 29.6		not broken
	PP (2-screw extr.	1174	/ 26.0 / >100	1080	/ 33.5		not broken
15	PP/30	2365	/ 33.0 / 2.6	2487	/ 47.6		9.2
	PP/30/D 2	1895	/ 31.1 / 4.7	2001	/ 46.5		11.3
	PP/30/D 5	1466	/ 26.0 / 8.4	1324	/ 36.0		30.7
20	PP/30/D 10	1192	/ 22.6 / 12.2	1044	/ 30.5		44.6
	PP/20	1634	/ 29.5 / 6.8	1621	/ 40.4		17.1
25	PP/20/D 3	1264	/ 25.2 / >100	1302	/ 35.4		(54.4) * not all broken!
	PP/20/D 7	962	/ 21.0 / >100	878	/ 27.0		not broken
30	E(MPa) = elastic modulus; σ (MPa) = maximal strength; ϵ (%) stain at break						

It appears from the table that the impact strength of the blends are greatly improved by the addition of the compatibilizer. The impact strength of blend PP/30/D 2 is over 22 % better than that of the corresponding non-

5 compatibilized. Even greater improvements were obtained with blends PP/30 D 5 and PP/30 D 10. Although the tensile and flexural strengths and thus also the moduli of elasticity of the blends were to some extent impaired by high

10 compatibilizer concentrations, by a moderate dosage (5 wt.-% of the compatibilizer at the most), while maintaining a good impact strength level (i.e. Charpy > 30 kJ/m²), better strength and flexural properties were obtained than for the polymer matrix as such.

15 The micrographs (Figs. 1a and 1b) show that the compatibilizer also has a strong dispersive effect.

For extruded PP/LCP blends better tensile strengths were obtained when the draw ratio increased because the LCP phases

20 were subjected to deformation, upon which they formed fibres. This fact is evidenced by Figure 2.

Viscosity measurements show that the addition of LCP diminishes the melt viscosity of thermoplastics (such as

25 polypropylene in this Example). In spite of its small viscosity, compatibilizer D increases the viscosity of the blend towards the polypropylene level (Figure 3). This suggests an increased interaction between the blend components (possibly a chemical reaction).

30

Example 2 (comparison)

An attempt was made to improve the impact strength of PP/LCP

35 blends with the help of a non-functional terpolymer. According to a first embodiment, LCP was blended into a PP/EPDM (75/25) compound and, according to a second

embodiment, 5, 10, and 20 wt.-% of EPDM were added to PP/30 wt.-% LCP blends. The blends were processed, injection moulded, and tested as described above. The test results are given in Table 2.

Table 2. Mechanical properties of injection moulded PP/LCP/EPDM blends

5	Material	TENSILE PROPERTIES E (MPa) / σ (MPa) / ϵ (%)	FLEXURAL PROPERTIES E (MPa) / σ (MPa)	IMPACT STRENGTH Charpy (kJ/m ²)
10	PP	1047 / 24.0 / >100	964 / 29.6	not broken
	PP/20	1634 / 29.5 / 6.8	1621 / 40.4	17.1
	PP/30	2365 / 33.0 / 2.6	2487 / 47.6	9.2
15	PP/LCP/EPDM blends:			
	PP/30/EPDM 5	2385 / 30.9 / 3.1	2549 / 42.4	8.3
	PP/30/EPDM 10	2151 / 28.2 / 3.2	2415 / 39.8	8.4
20	PP/30/EPDM 20	1796 / 22.1 / 6.7	1778 / 29.5	12.1
	PP/EPDM(75/25) compound + LCP:			
25	PP-comp.	627 / 12.4 / >110	622 / 17.0	not broken
	PP-comp./30	2013 / 26.4 / 2.5	2157 / 33.4	8.7
30	PP-com./PP//30 (50/50)	2149 / 31.8 / 2.7	2574 / 41.3	8.5

E(MPa) = modulus of elasticity; σ (MPa) = maximal strength; ϵ (%) strain at break

As apparent from the table an increase of the amount of the soft EPDM rubber caused a further slight weakening of the tensile and flexural strength properties of the blends. The impact strength of the blends did not, however, improve as expected. The micrographs indicate a smooth dispersion of the small rubber particles (0.5 to 1 mm) into the PP matrix. The non-functional rubber particles are not located on the interfaces between the LCP and PP phases, which means that the necessary interaction between the phases was not achieved.

This strengthens the basic concept that the activity of the rubber compatibilizer (D) is specifically based on a chemical reaction, because a similar effect is not obtained with rubber only.

Example 3

Compatibilized PET/LCP blends

Polymer blends were prepared from a PET polymer and LCP and 2, 5, and 10 wt.-% of reactive ethylene-based terpolymers (comp. D) or maleic acid grafted SEBS block copolymer (comp. A). The preparation of the blends, the injection moulding, and the testing thereof were carried out as described above.

The results are shown in Figures 5 to 7.

Figure 5 shows that the impact strength of the PET/LCP 10 blend was increased with both compatibilizers. Already at a 2 wt.-% terpolymer addition a clear increase in the impact strength could be noticed, and after a 5 wt.-% terpolymer addition only half of the test bars were broken. The impact strengths of these bars were 3.5 times greater than the strengths of uncompatibilized samples. By a 10 wt.-% addition the impact strength was raised to the same level as the impact strength of the matrix polymer. Also at a 10 wt.-%

block copolymer addition only half of the test bars were broken. The impact strength of these bars was 2.4 times greater than that of uncompatibilized samples.

5 The changes in the flexural and tensile strengths subject to compatibilizer additions are shown in Figures 6 and 7.

10 Surprisingly, it can be noted that during tensile and flexural tests the moduli of elasticity of the blends were clearly better than the corresponding values of the polymer matrix at a 2 % terpolymer addition. Because the impact strength at the same addition amount was about 35 kJ/m², a rather advantageous polymer blend was obtained with this compatibilizer addition.

15

Example 4

Binary blends of LCP and compatibilizers

20 A. Preparation

Binary blends of LCP and some compatibilizers were made in order to characterize the interactions between the compatibilizers and the LCP. In addition, a novel way of
25 blending was also studied by preblending the compatibilizer and LCP first, and by adding the thermoplastics later in a second blending stage. The idea was to give the compatibilizer a better possibility to interact with the LCP.

30 The following binary blends were first made:

B1. PP / Comp. D (80/20)

B2. Vectra A950 / Comp. D (80/20)

B3. Vectra A950 / Comp. A (80/20)

35

and in the second stage polypropylene (PP) and/or poly(ethylene terephthalate) (PET) were added to blends B2

and B3, such that blends were provided having 30 percent by weight of the LCP and 5 to 7.5 percent by weight of the compatibilizer.

- 5 B2PP Vectra A950 / Comp. D (80/20) + PP (VB1950K)
- B2PET Vectra A950 / Comp. D (80/20) + PET (Arnite D04300)
- B3PET Vectra A950 / Comp. A (80/20) + PET (Arnite D04300)

10 The melt blending was carried out with a DSK 42/7 counter-rotating twin-screw extruder at about 290 °C (230 °C for B1) with a screw speed of 75 rpm. After drying, the blends were injection moulded to form test specimens for testing of mechanical properties.

15 The results were compared to those of the blends having similar compositions but being prepared in the traditional way by first mixing all three components and then blending them in the extruder.

20 It should be emphasized that the counter-rotating twin-screw extruder used for the binary blends is not so good mixing equipment as the co-rotating one used for the blends described in the previous examples.

25 B. Morphology and rheology of the binary blends

 Compatibilizer D was dispersed in the PP phase as fine droplets of the order of less than 1 μm (Fig. 8a). Partly because of the large proportion of the LCP, the binary blend
30 of comp. D and LCP exhibited a fibrous structure. The compatibilizer could not be seen as a separate phase on the micrographs, and it is possible that it reacted so well with the LCP that it did not form a separate phase (Fig. 8b).
 Compatibilizer D raised the melt viscosity of the LCP to a
35 clearly higher level (Fig. 9) which seems to indicate a chemical reaction between the compatibilizer and LCP as suggested also in earlier examples. On the other hand the

addition of Comp. D to PP (blend B1) did not have any influence on the melt viscosity of PP. Thus, the effectiveness of compatibilizer D in compatibilization of LCP and PP is based on good mixing of comp. D in the PP matrix and chemical reactivity with the LCP.

The blend LCP / Comp. A was also extremely fibrous due to the high amount of LCP, and its structure was possibly more reminiscent of a LCP (Figure 8c). However, the viscosity of the LCP did not increase at all after addition of comp. A, which means that there was not a same kind of interaction between A and the LCP as between D and the LCP.

C. Compatibilized blends of LCP/PET and LCP/PP

Mechanical properties and morphology

Both compatibilizers (A and D) improved the flexural properties of LCP/PET blends as seen in Table 3.

Table 3. Elastic modulus (E), strength (σ) and displacement at yield ($\epsilon\gamma$) (three-point-bending, 5 mm/min).

Material	E (MPa)	σ (MPa)	$\epsilon\gamma$ (mm)
PET	2346	77	8.3
PET/30	3009	83	-* not measured
B2PET	4103	91	7.7 (PET/30 LCP/5.0 D)
B3PET	3673	86	8.1 (PET/30 LCP/7.5 A)

Morphology of the extruded blends is presented by SEM micrographs in Fig. 10. Blend B2PET exhibited a highly fibrillar structure throughout the sample, which explains the high level of strength and stiffness, while B3PET contained deformed LCP domains but less fibres than B2PET. In addition,

the LCP domains (fibres) were better attached to the PET matrix and the fibre surfaces were not so smooth in B2PET due to the more reactive compatibilizer.

5 Tensile and impact strength properties of PP/LCP blends are shown in Table 4. Significant improvement in impact strength was achieved again by compatibilizer D, while the values of strength and modulus were slightly decreased in comparison to
10 the uncompatibilized blend. The impact strength of B2PP was also better than that of the similar blend composition prepared in the traditional way (PP/30/D5 in Table 1).

Thus preblending of LCP and the compatibilizer before the addition of the thermoplastic matrix polymer may be
15 advantageous for the resultant blend properties.

Table 4. Tensile and impact properties of PP/LCP blends.

20	Material	E (MPa)	σ (MPa)	ϵ (%)	Charpy Impact Strength (kJ/m ²)
	PP	1047	24	>100	not broken
	PP/30	2365	33	2.5	9.2
25	B2PP*	1332	26	5.9	39.2

*PP/30 % LCP/ 5 % comp. D

30

In the blend B2PP LCP formed fiber-like domains which were rather well attached to the matrix as seen in Fig. 10c.

Claims:

1. A polymer blend containing
 - 95 to 5 parts by weight of a matrix polymer,
 - 5 - 5 to 50 parts by weight of a liquid crystalline polymer, and
 - 0.1 to 30 percent by weight of a substance (compatibilizer) promoting the compatibility of the polymer matrix and the liquid crystalline component,
 - 10 the amount of the compatibilizer being calculated on basis of total amount of the matrix polymer and the liquid crystalline polymer,
 - characterized in that
 - said compatibility promoting substance consists of a
 - 15 polymer containing reactive functional groups, and
 - the tensile strength and flexural strength of the blend are better than the corresponding properties of the matrix polymer, and its Charpy impact strength is at least 20 % better than that of the
 - 20 corresponding uncompatibilized blend.
2. The polymer blend according to claim 1, wherein the Charpy impact strength of the polymer blend is at least 30 kJ/m² determined according to the Standard ISO 179.
- 25 3. The polymer blend according to claim 1, wherein the amount of the liquid crystalline polymer is about 10 to about 30 percent by weight of the total amount of the matrix polymer and the liquid crystalline polymer.
- 30 4. The polymer blend according to any one of the previous claims, wherein the functional groups of the compatibilizer are selected from the group comprising carboxylic acid, anhydride, epoxy, oxazolino, hydroxyl, isocyanate,
- 35 acetylacetam, and carbodiimide groups, or mixtures thereof.
5. The polymer blend according to claim 4, wherein the

functional groups of the compatibilizer comprise glycidyl methacrylate and/or epoxy groups.

5 6. The polymer blend according to any of the previous claims, wherein the amount of functional groups is about 0.1 to 30 % of the compatibilizer.

10 7. The polymer blend according to any of the previous claims, wherein the matrix polymer comprises polyolefins, in particular polypropylene or polyethylene or copolymers thereof, or a polyester, in particular poly(ethylene terephthalate or poly(butylene terephthalate)).

15 8. The polymer blend according to claims 6 or 7, wherein the compatibilizer comprises a SEBS polymer functionalized with maleic anhydride or an olefin polymer functionalized with glycidyl methacrylate.

20 9. The polymer blend according to claim 1, in which the polymer matrix comprises polypropylene (PP),
c h a r a c t e r i z e d in that the liquid crystalline polymer (LCP) is a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid and the compatibilizer comprises a
25 ethylene terpolymer (Comp. D) with glycidyl methacrylate groups as reactive groups, the blend containing about 70 parts by weight of PP, about 30 parts by weight of LCP, and 5 to 10 percent by weight of Comp. D (calculated on basis of the total amount of PP and LCP), or about 90 parts by weight of PP, about 10 parts by weight of LCP, and 2 to 5 percent by
30 weight of Comp. D (calculated on basis of the total weight of PP and LCP).

35 10. The polymer blend according to claim 1, in which the polymer matrix comprises poly(ethylene terephthalate) (PET),
c h a r a c t e r i z e d in that the liquid crystalline polymer (LCP) is a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid and the compatibilizer comprises a

ethylene terpolymer (Comp. D) with glycidyl methacrylate groups and epoxy groups as reactive groups, the blend containing about 90 parts by weight of PET, about 10 parts by weight of LCP, and 2 to 5 percent by weight of Comp. D
5 (calculated on basis of the total amount of PET and LCP).

11. The polymer blend according to claim 1, in which the polymer matrix comprises poly(ethylene terephthalate) (PET), characterized in that the liquid crystalline
10 polymer (LCP) is a copolymer of hydroxynaphthoic acid and hydroxybenzoic acid and the compatibilizer (Comp. A) comprises maleic anhydride grafted SEBS, the blend containing about 90 parts by weight of PET, about 10 parts by weight of LCP, and 5 to 10 percent by weight of Comp. A (calculated on
15 basis of the total amount of PET and LCP).

12. The polymer blend according to any one of claims 1 to 11, wherein it is in the form of a pipe tube sheet film or fibre.

20 13. Process for preparing a liquid crystalline polymer blend, characterized by melt mixing

- 95 to 5 parts by weight of a matrix polymer,
- 5 to 50 parts by weight of a liquid crystalline polymer, and
- 25 - 0.1 to 30 percent by weight of functional polymer (calculated on basis of the total amount of the matrix polymer and the liquid crystalline polymer) in order to form a compatibilized polymer blend, whose Charpy impact strength is at least 20 % better
30 than that of the corresponding uncompatibilized blend and
- optionally subjecting the blend obtained to further processing.

35 14. The process according to claim 13, wherein the compatibilizer is first preblended with the liquid crystalline polymer, and then a thermoplastic component is

added and the melt mixing is carried out.

5 15. The process according to claims 13 or 14, wherein the liquid crystalline polymer blend is subjected to extrusion in order to increase the longitudinal strength of the blend.

10 16. The process according to claim 15, wherein, in connection with the extrusion, the transversal strength of the liquid crystalline polymer blend is increased.

17. The process according to claim 16, wherein extrusion is carried out by using rotary dies or equivalent means.

15 18. Constructional parts of electrical and optical cables, characterised in that they consist at least partially of a blend according to any one of claims 1 to 11.

20 19. Injection moulded blow moulded and deep drawn products, characterised in that they consist at least partially of a blend according to any one of claims 1 to 11.

1/7

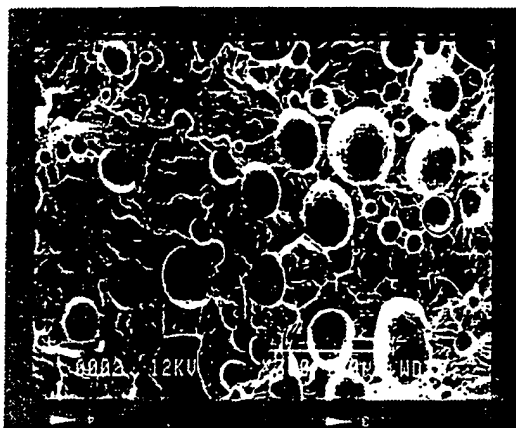


Fig. 1a

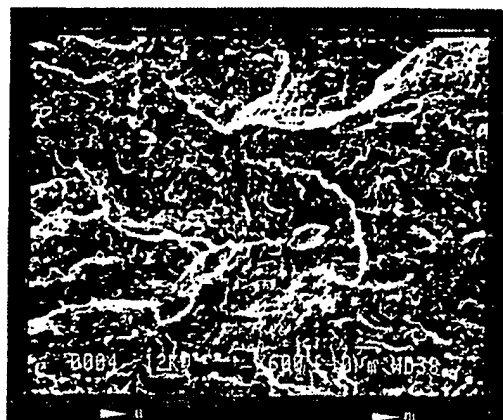


Fig. 1b

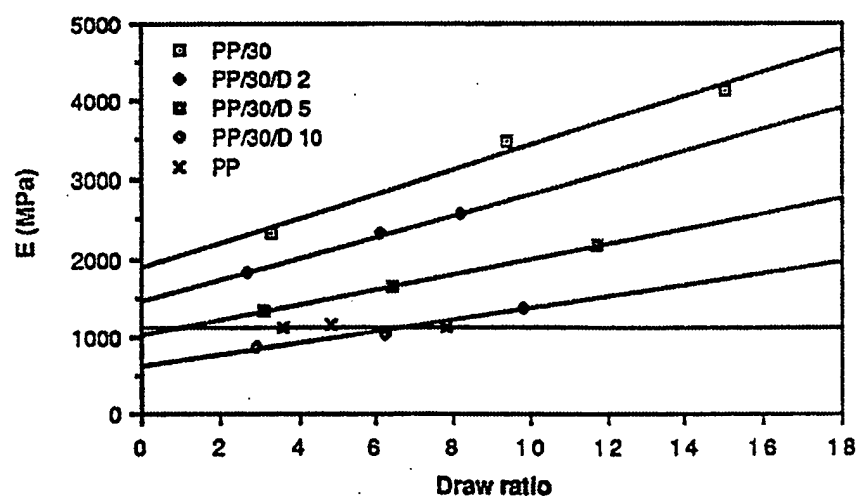


Fig. 2

SUBSTITUTE SHEET

2/7

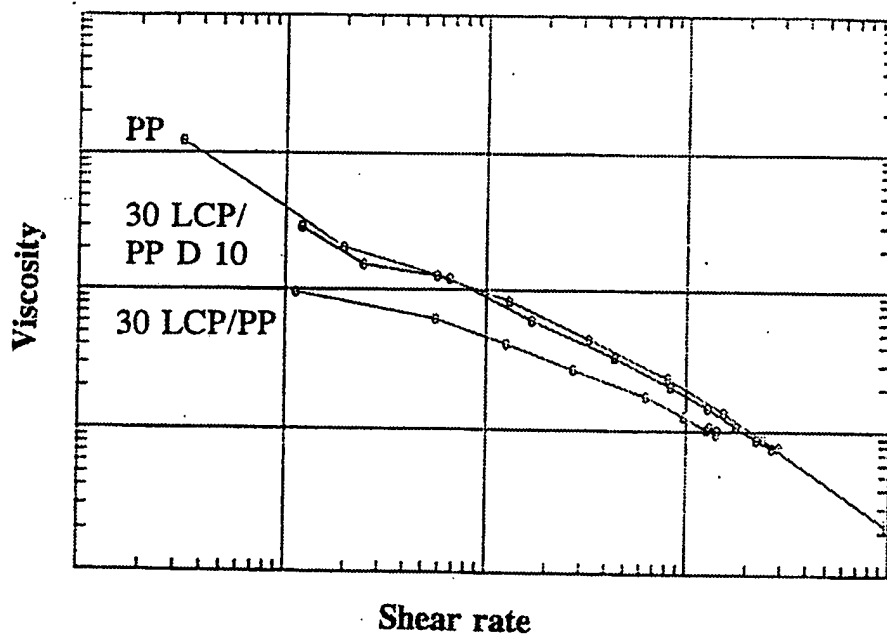


Fig. 3



Fig. 4a

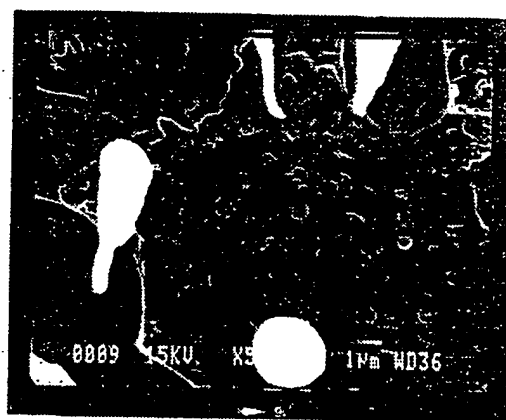


Fig. 4b

3/7

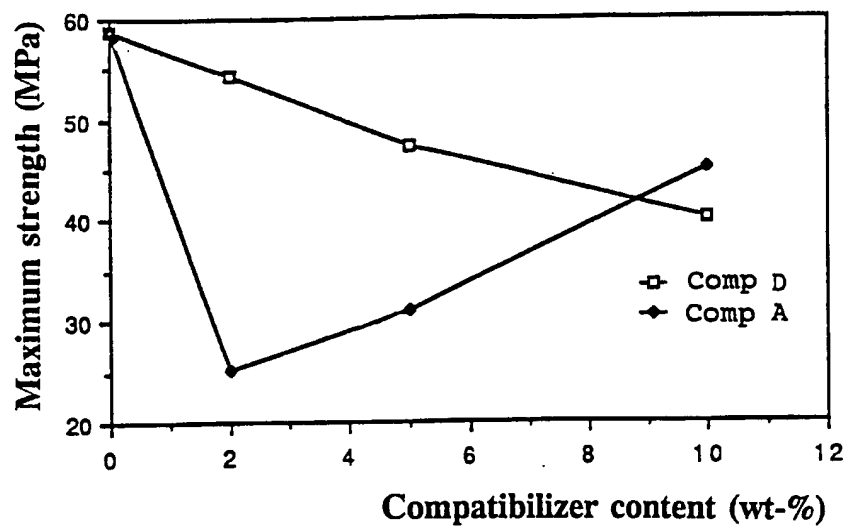


Fig. 5

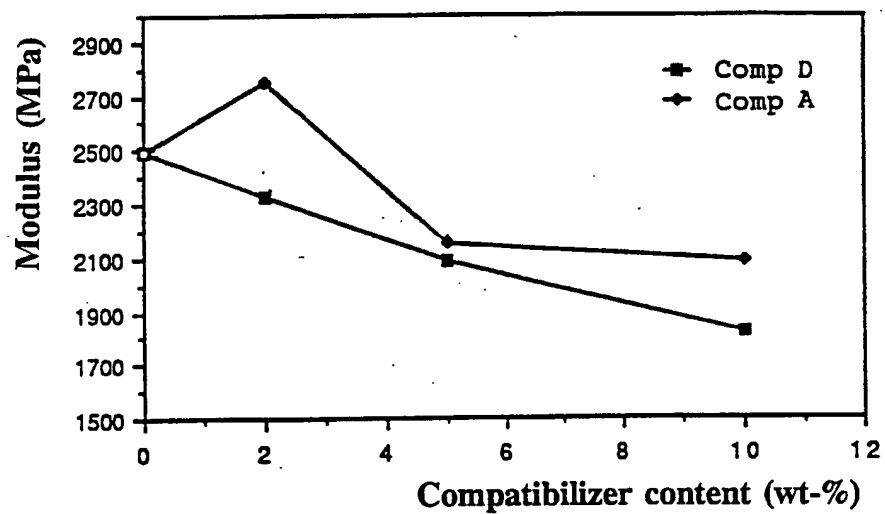


Fig. 6

4/7

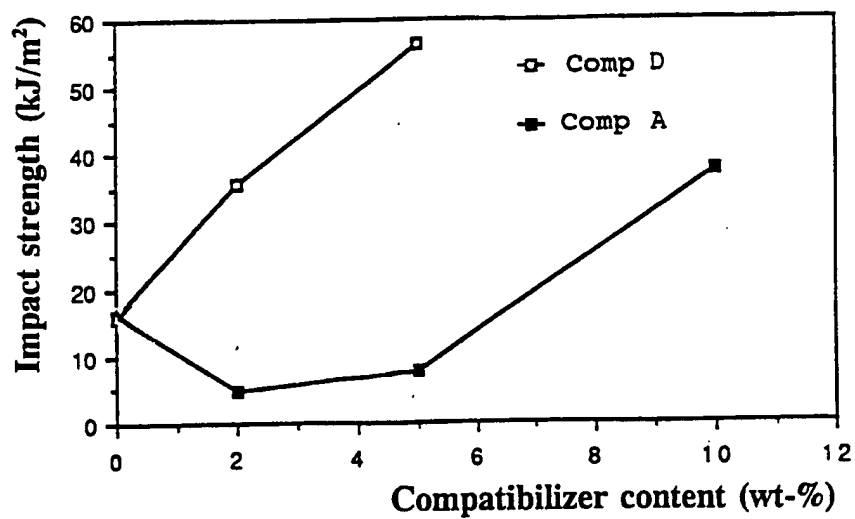


Fig. 7

5/7

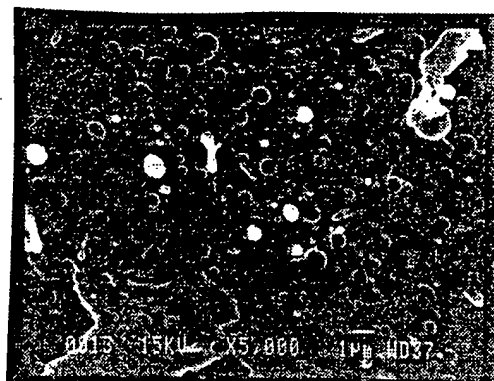


Fig. 8a

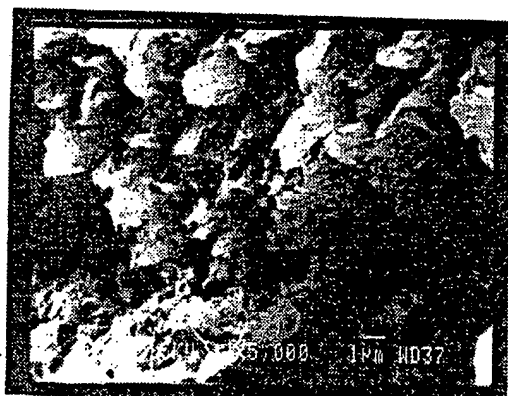


Fig. 8b

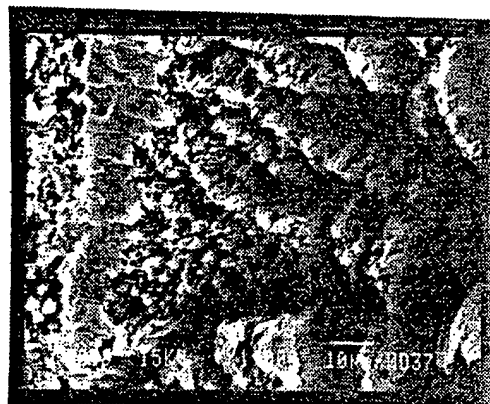


Fig. 8c



Fig. 8d

6/7

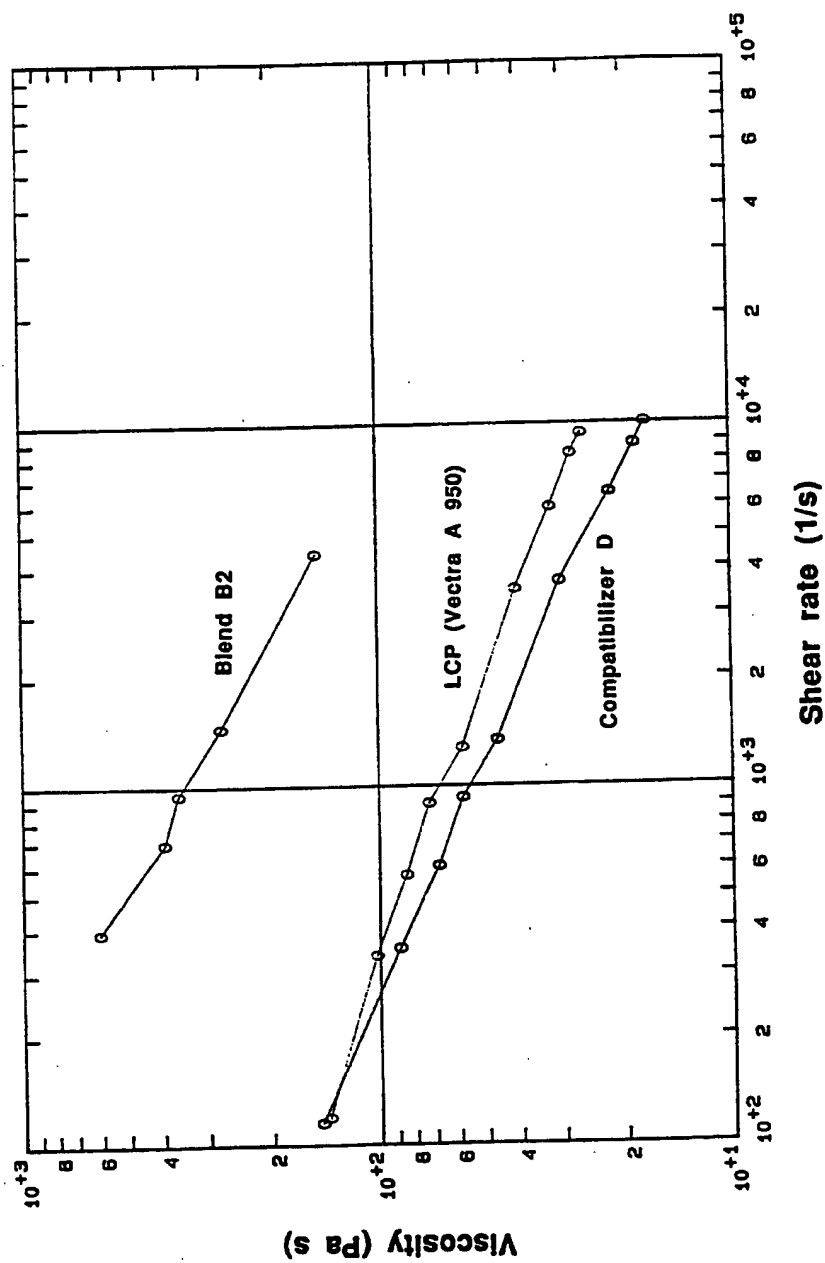


Fig. 9

7/7

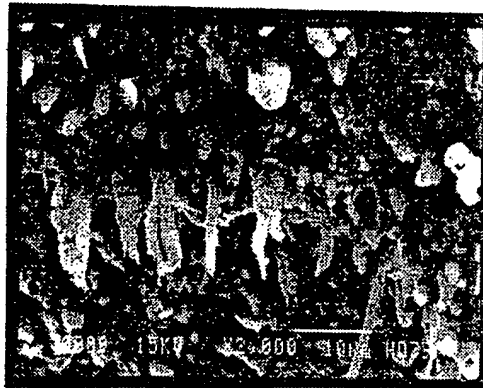


Fig. 10a

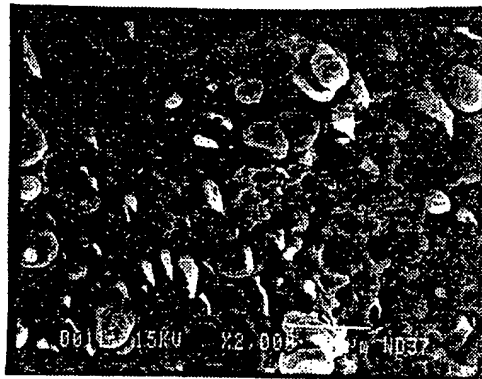


Fig. 10b

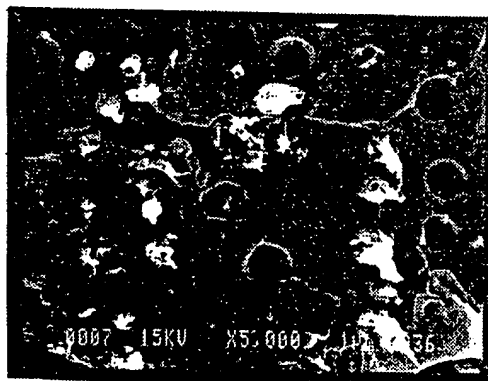


Fig. 10c

INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 93/00233

A. CLASSIFICATION OF SUBJECT MATTER

IPC5: C08L 101/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC5: C08L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPI, CA

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP, A2, 0380112 (KAWASAKI STEEL CORPORATION), 1 August 1990 (01.08.90) --	1-19
X	Chemical Abstracts, Volume 115, No 12, 23 Sept 1991 (23.09.91), (Columbus, Ohio, USA), Heino, M et al, "Blends of a thermotropic liquid crystalline polymer and some thermoplastics. Compatibilizing and production of polymer blends", page 41, THE ABSTRACT No 115652z, Gov.Rep.Announce Index 1990, 90 (24) --	1-19
P,X	WO, A1, 9218568 (VIRGINIA POLYTECHNIC INSTITUTE AND STATE UNIVERSITY), 29 October 1992 (29.10.92) -- -----	1-19

☐ Further documents are listed in the continuation of Box C.☒ See patent family annex.

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Date of the actual completion of the international search

31 August 1993

Date of mailing of the international search report

02 -09- 1993

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INTERNATIONAL SEARCH REPORT

Information on patent family members

30/07/93

International application No.

PCT/FI 93/00233

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A2- 0380112	01/08/90	CA-A- 2008538 JP-A- 2276854	26/07/90 13/11/90
WO-A1- 9218568	29/10/92	NONE	